

CONTINUOUS-TIME DEADBEAT OBSERVATION PROBLEM

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ABSTRACT

Two observers are shown to estimate the states of a linear dynamic system deadbeatly in continuous time.

The first observer uses a finite number of delayed input/output measurements to reconstruct the state vector with zero error being provided with a process history over its largest time-delay. Moreover, the largest time-delay value puts a natural limit to the observer memory. The second observer comprises a conventional Luenberger observer and a finite-memory deadbeat observer to achieve zero estimation error at finite time.

INTRODUCTION

It is well known that deadbeat performance can be achieved in discrete-time systems by placing all roots of the characteristic polynomial of an observer or controller at the origin. Therefore, any pole-placement design technique provides the desired transient response property. In contrast, continuous-time deadbeat problem does not naturally arise from pole placement and has drawn serious research attention only recently. As it can be seen, the continuous-time deadbeat controllers and observers for the plants described by ordinary linear differential equations belong to another, as the plants, class of dynamic systems. Presence of time delays in the control law or observer structure becomes inevitable to drive control or observation error to zero deadbeatly. Hence, continuous-time deadbeat structures are governed rather by differential-difference than ordinary differential equations and crave a special consideration.

Being a new research area, continuous-time deadbeat problem is treated only in a few papers. In [1, 2], finite-memory deadbeat observation problem

has been solved by a direct state-space approach related to deterministic least squares. Unfortunately, enough, the resulting observer works in the open-loop mode only. In [3], a general solution for the deadbeat tracking and stabilization problems is obtained via finite Laplace transform, a technique common to differential-difference equations theory.

In the present paper, we develop a deadbeat observer for multivariable continuous systems to be used in a feedback control structure. The paper is composed as follows. Firstly, we describe the Finite-Memory Deadbeat Observer (FMDO) using a different, than it is in [2], approach. Then, a combination of a conventional Luenberger observer and FMDO is exploited to achieve desired performance in an Infinite-Memory Deadbeat Observer (IMDO). It is shown that the IMDO estimate can be used in feedback control since the time-delay part of the observer is introduced in a way which does not change the closed-loop stability properties.

1. FINITE-MEMORY OBSERVER

Let us consider the nonhomogeneous equation

$$\begin{aligned}\dot{x}(t) &= Ax(t) + Bu(t) \\ y &= Cx(t)\end{aligned}\quad (1)$$

where $x(t) \in R^n$ is the state vector, $u(t) \in R^m$ is the control vector, and $y(t) \in R^l$ is the observation vector. A, B, C are real matrices of appropriate dimensions.

Theorem 1: Provided that the matrix

$$W_k = \sum_{i=0}^k \exp(-A^T \tau_i) C^T C \exp(-A \tau_i)$$

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is positive definite, then the observer

$$\begin{aligned}\hat{x}_k(t) = & W_k^{-1} \sum_{i=0}^k \exp(-A^T \tau_i) C^T (y(t - \tau_i) \\ & + \int_{t-\tau_i}^t C \exp(A(t - \delta - \tau_i)) B u(\delta) d\delta) \end{aligned} \quad (1.2)$$

has the following properties (i) finite memory, limited by the largest time-delay τ_k ; (ii) dead-beat performance, i.e. $e(t) = x(t) - \hat{x}(t) = 0$; $t > \tau_k$ for any initial function $\phi_0 = y(t)$, $t \in [-\tau_k, 0]$.

Proof: Omitted.

Positive definiteness of the W_k matrix guarantees [1] that the system (1.1) (which is a time-delay system) is spectrally observable. In the case $\det(W_k) = 0$, the observer (1.2) becomes a least-squares estimator without the deadbeat property, since it reconstructs the state vector only partly.

It is worth noting that whereas the only design parameter for a deadbeat observer is the sampling period, the finite-memory observer (1.2) has its parameters fully defined by a set of time delays τ_i , $i = 0, \dots, k$ which might be chosen by some relevant procedure considering for example observer's robustness against model uncertainties, optimality etc.

As Theorem 1 shows, there were no limitation on the choice of τ_i but positive definiteness of W_k , and, hence, they may be taken arbitrarily as commensurate or noncommensurate positive reals. This becomes a merit of the method in comparison with the finite Laplace transform design procedure [3] which tackles only commensurate time delays.

Taking Laplace transform of (1.2) yields

$$\begin{aligned}\hat{x}_k(s) = & W_k^{-1} \sum_{i=0}^k \exp(-A^T \tau_i) C^T C \exp(-s\tau_i) \times \\ & (x(s) + (sI - A)^{-1} B u(s)) - (sI - A)^{-1} B u(s)\end{aligned}$$

which hints to the conclusion that the applicability of FMDO to feedback control is questionable. Indeed, had $\hat{x}_k(s)$ been fed back as $u(s) = G\hat{x}_k(s)$, would all the time delays τ_i appear in the characteristic polynomial of the closed loop system. Of course, it does not necessarily mean poor stability, but rather makes the task of procuring reasonable transient behavior more complicated.

2. INFINITE-MEMORY OBSERVER

Continuous-time deadbeat phenomenon is not bound only to finite-memory structures, but can be also accomplished in infinite-memory structures.

Theorem 2: Provided that the matrix $(A - KC)$ is Hurwitz and the matrix

$$W_k = \sum_{i=0}^k \exp((KC - A)^T \tau_i) C^T C \exp((KC - A) \tau_i)$$

is positive definite, then the observer

$$\begin{aligned}\dot{\hat{x}}(t) = & \bar{x}(t) + e_d(t) \\ \dot{\hat{x}}(t) = & A\hat{x}(t) + Bu(t) + K(y(t) - C\hat{x}(t)) \\ e_d(t) = & W_k^{-1} \sum_{i=0}^k \exp(-(A - KC)^T \tau_i) C^T \times \\ & (y(t - \tau_i) - C\hat{x}(t - \tau_i))\end{aligned} \quad (2.1)$$

is a deadbeat observer in the sense that the estimation error $e(t) = x(t) - \hat{x}(t)$ is zero for all $t \geq \tau_k$.

Proof: Omitted.

Strictly speaking, it is not necessary to impose the stability limitation on the matrix $(A - KC)$ since the FMDO is as well able to reconstruct the state vector of an unstable system. However, from a practical standpoint, the presence of unbounded signals in a observer seems to be irrational.

As it follows from (1.2), the FMDO structure cannot be directly used for feedback control as feedback closed-loop stability is not guaranteed. The following theorem shows that the IMDO structure overcomes this difficulty.

Theorem 3: Suppose the feedback control law

$$u(t) = G\hat{x}(t) \quad (2.2)$$

is used to stabilize the plant (1.1). Then, the closed-loop system (1.1), (2.1), (2.2) is asymptotically stable iff $(A - KC)$ and $(A + BG)$ are Hurwitz matrices.

Proof: Omitted.

The observer-based control system (2.2), (2.1), in comparison with the conventional feedback control $u(t) = G\bar{x}(t)$, retains closed-loop stability and simultaneously improves transient response of the control loop attaining the plant state vector perfectly follow the model

$$\dot{\hat{x}}(t) = (A + BG)x(t)$$

after the deadbeat settling time τ_k has been expired. In this sense, the deadbeat observer compensates additional transient effects caused by the Luenberger observer. This can be also illustrated by evaluating the closed-loop transfer function.

Theorem 4: With the control law

$$u(t) = G\hat{x}(t) + r(t)$$

used for the system (1.1), (2.1), the closed-loop transfer function is given by

$$y(s) = C(sI - A - BG)^{-1} B r(s)$$

Proof: Omitted.

Thus, observer's own dynamics is cancelled in the closed-loop transfer function and does not affect controller performance, provided transient response in IMDO settled deadbeatly.

4. CONCLUSIONS

A deadbeat observation problem is solved for continuous linear multivariable systems. Two deadbeat observers possessing respectively finite and infinite process memory are introduced.

The memory limit imposed intrinsically by the finite-memory observer structure might be helpful in preventing it from possible divergence and makes observer residuals more sensitive to recent measurements.

The infinite memory deadbeat observer is shown to improve the controller performance in a feedback control system by effectively cancelling the control error transient terms caused by observer dynamics.

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