

Trajectory Initialization in Adaptive Nonlinear Control *

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Submitted to *1993 IEEE Mediterranean Symposium
on New Directions in Control Theory and Applications*

Keywords: Adaptive control, nonlinear systems, tracking, initialization, transient performance.

Abstract

Transient performance is a critical issue that has only recently started receiving some attention in the adaptive control literature. In this paper, we focus on a very simple means of improving transient performance and reducing control effort: *initialization of the reference trajectory*. Using available information about the initial state of the plant, it is always possible to design a reference trajectory which minimizes the initial values of the error variables in the adaptive system. In the case of model reference control, this is achieved by adjusting the initial conditions of the reference model. If, on the other hand, the reference trajectory is given as a precomputed function of time, then it can be initialized through the addition of exponentially decaying terms which define the *reference transients*.

While it is not clear that traditional adaptive schemes, which only guarantee convergence of the tracking error to zero, benefit from trajectory initialization, such an initialization offers

*This work was supported in part by the National Science Foundation under Grant ECS-91-96178, in part by the Air Force Office of Scientific Research under Grant AFOSR 92-J-0004, and in part by a UCLA Faculty Development Award.

ve controllers introduced in our recent
al stability and tracking for linear and
eters. Furthermore, they guarantee con-
manifold, on which only the parameter
g convergence property is owed to the
nstruction of a full Lyapunov function

for initialization. It is comprised of
reference trajectory, so that its value at
ween the actual trajectory of the system
essentially places the initial point of
point of the system trajectory, thereby
turn results in a significant reduction
directly related to the initial value of

output-feedback designs, and show that
transient performance bounds) can be
system. Specifically, in the full-state-
initial parameter estimation error. In
reference output can be chosen to match
conditions of the reference trajectory
Lyapunov value to the sum of the initial
at any additional knowledge about the
the initialization procedure to further

consider a third-order example with
y φ is multiplied by an unknown pa-

(1)

(2)

from the stabilizing functions α_1 and α_2 . At
, at Step 2, we design α_2 as a control law for x_3 .
s designed at Step 3. The actual update law $\gamma\tau_3$
Step 3, while the intermediate update laws τ_1
g functions. The results of the design procedure

(3)

(4)

$$\frac{\partial \alpha_1}{\partial \hat{a}} \gamma \tau_2 + \frac{\partial \alpha_1}{\partial y_r} \dot{y}_r + \ddot{y}_r \quad (5)$$

(6)

$$\frac{\partial \alpha_2}{\partial z_2} \left(-z_1 - c_2 z_2 + z_3 + \frac{\partial \alpha_1}{\partial \hat{a}} \gamma \frac{\partial \alpha_2}{\partial z_1} \varphi z_3 \right) \dot{y}_r + \frac{\partial \alpha_2}{\partial \dot{y}_r} \ddot{y}_r + y_r^{(3)} \quad (7)$$

(8)

$$+ z_3^2) + \frac{1}{2\gamma} \tilde{a}^2, \quad (9)$$

ed-loop system is

$$z_2 z_2^2 - c_3 z_3^2 \leq 0. \quad (10)$$

rgo to the manifold $M = \{z_1 = 0, z_2 = 0, z_3 = 0\}$,
nzero is the parameter error \tilde{a} .

this case. From the definition (1) of the error
we see that by choosing

(11)

$$= x_3(0) + \frac{\partial \varphi}{\partial x_1}(y_r(0)) \hat{a}(0) \dot{y}_r(0),$$

$$0) = \frac{1}{2\gamma} \tilde{a}^2(0).$$

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